

Your Ref.: A/YL-KTS/1084

Our Ref.: P25012/TL26010

7 January 2026

The Secretary
Town Planning Board
15/F., North Point Government Offices
333 Java Road, North Point, Hong Kong

By E-mail
tpbpd@pland.gov.hk

Dear Sir,

Submission of Further Information (FI)

**Proposed Temporary Warehouse (excluding Dangerous Goods Godown)
With Ancillary Office and Associated Filling of Land for a Period of 3 Years in
“Agriculture” Zone, Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B,
1015 RP, 1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113,
Kam Tin, Yuen Long, New Territories
(Application No. A/YL-KTS/1084)**

We write to submit a revised drainage proposal (Plans 6.1b & 6.2b) and hydraulic calculations for the captioned application.

Yours faithfully,
For and on behalf of
Goldrich Planners & Surveyors Ltd.

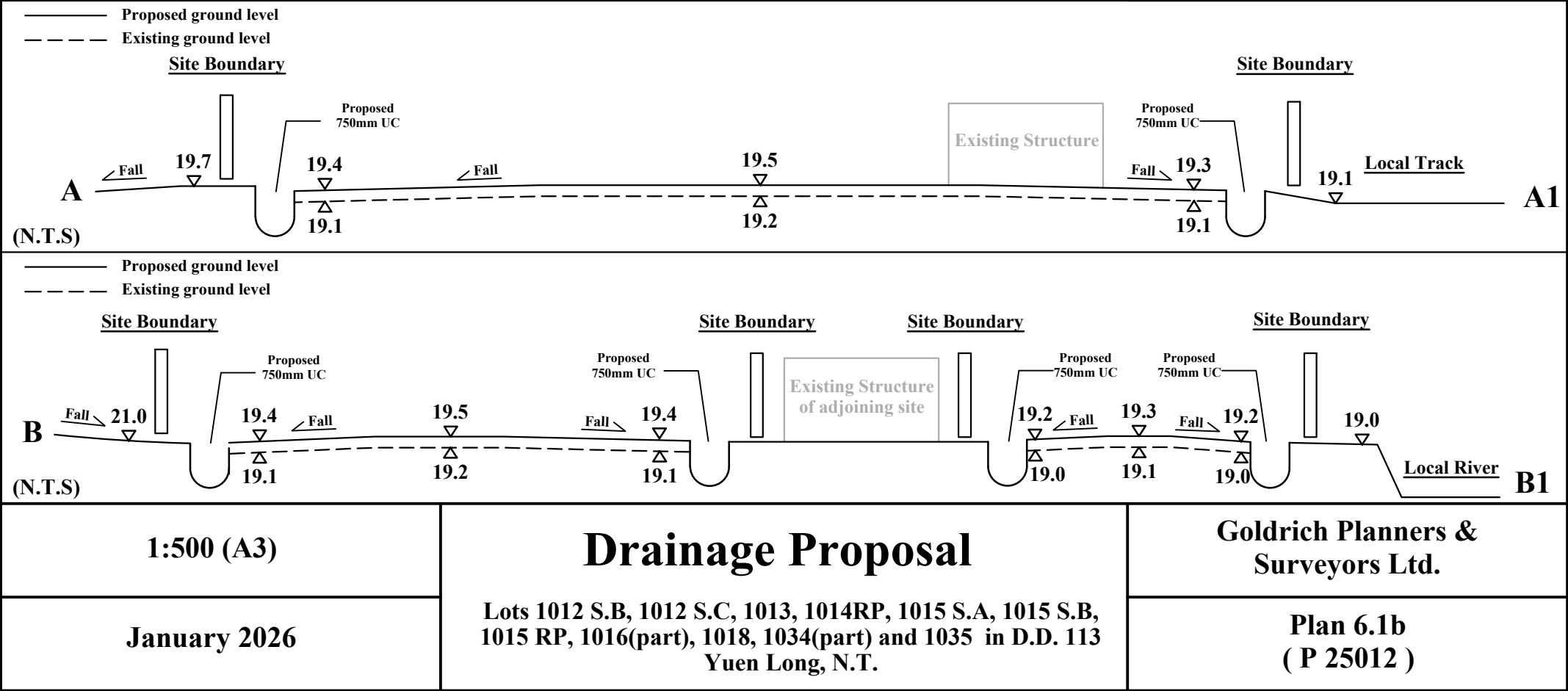
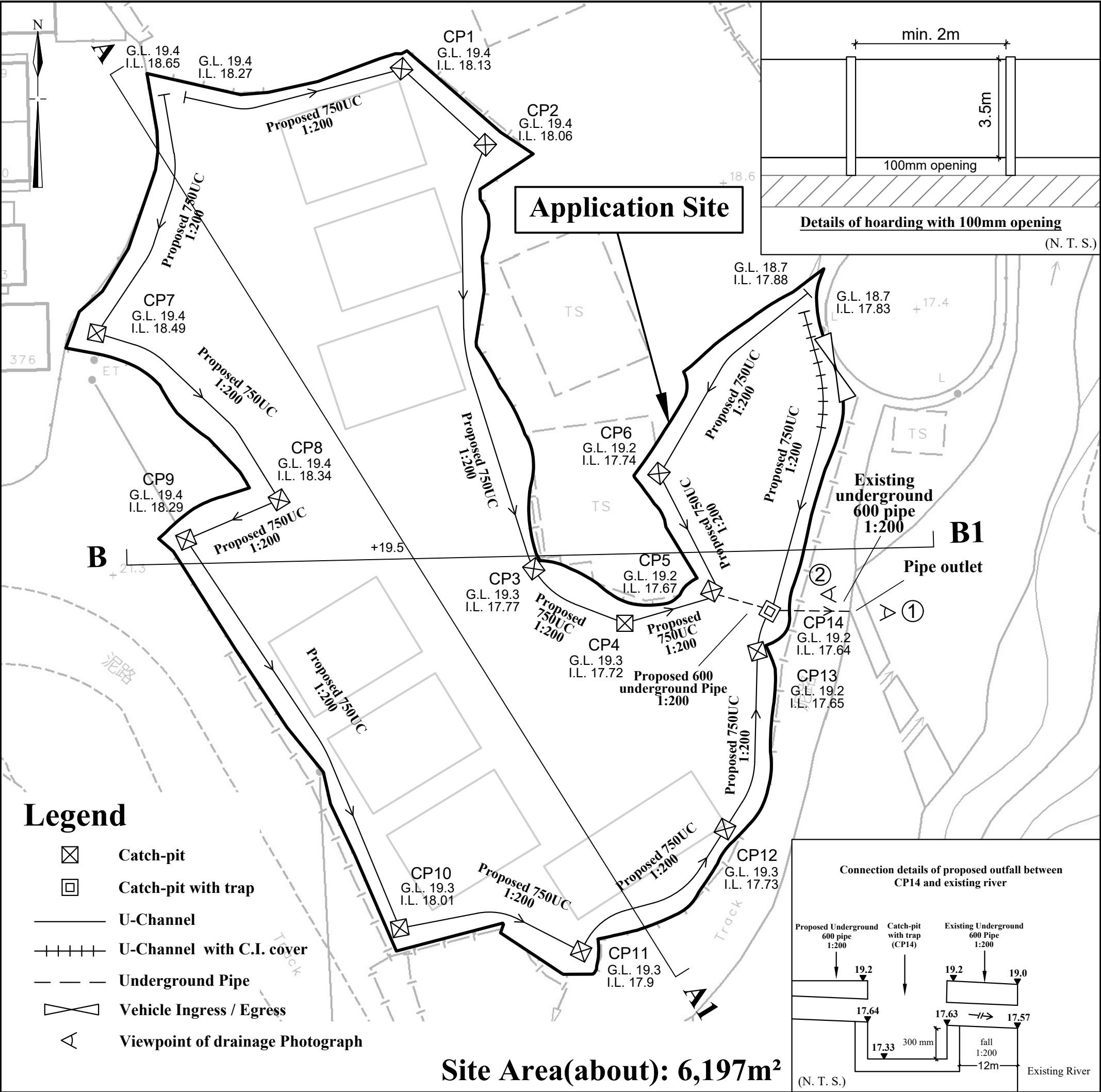


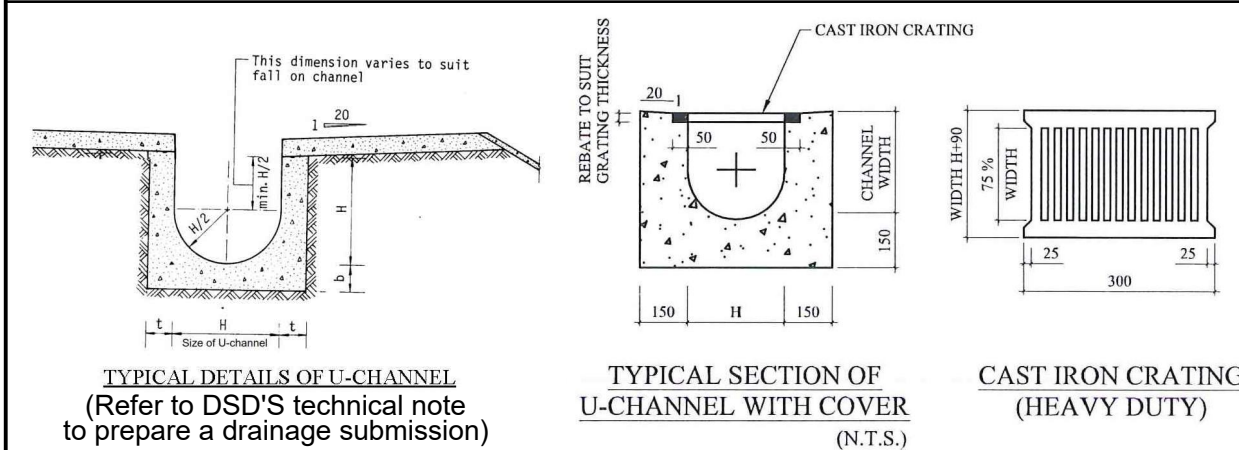
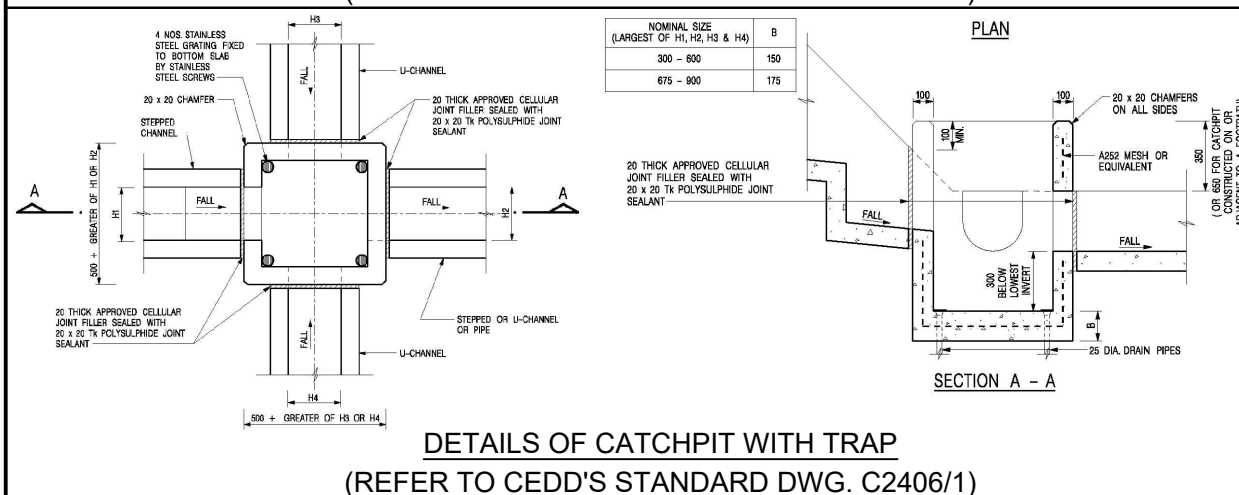
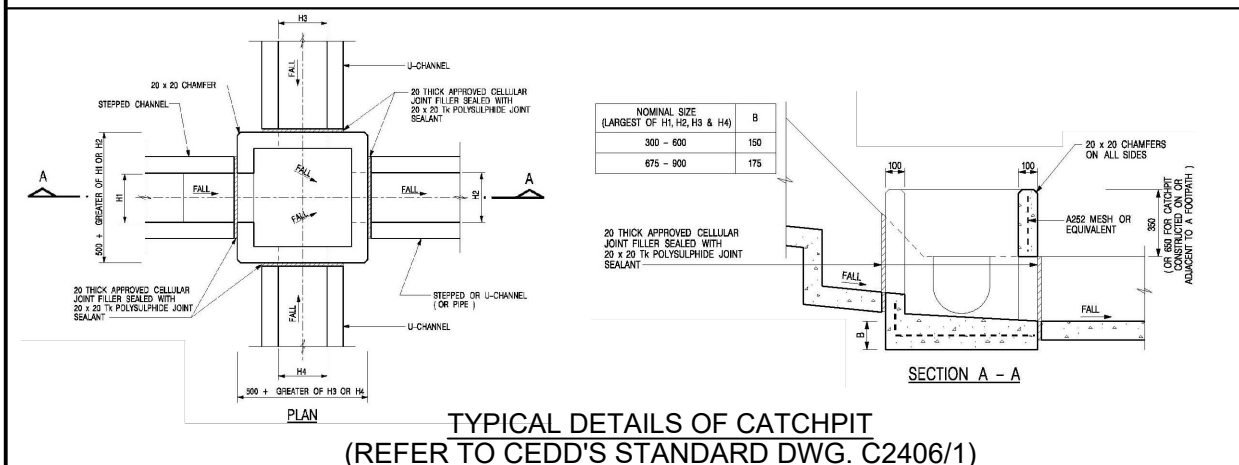
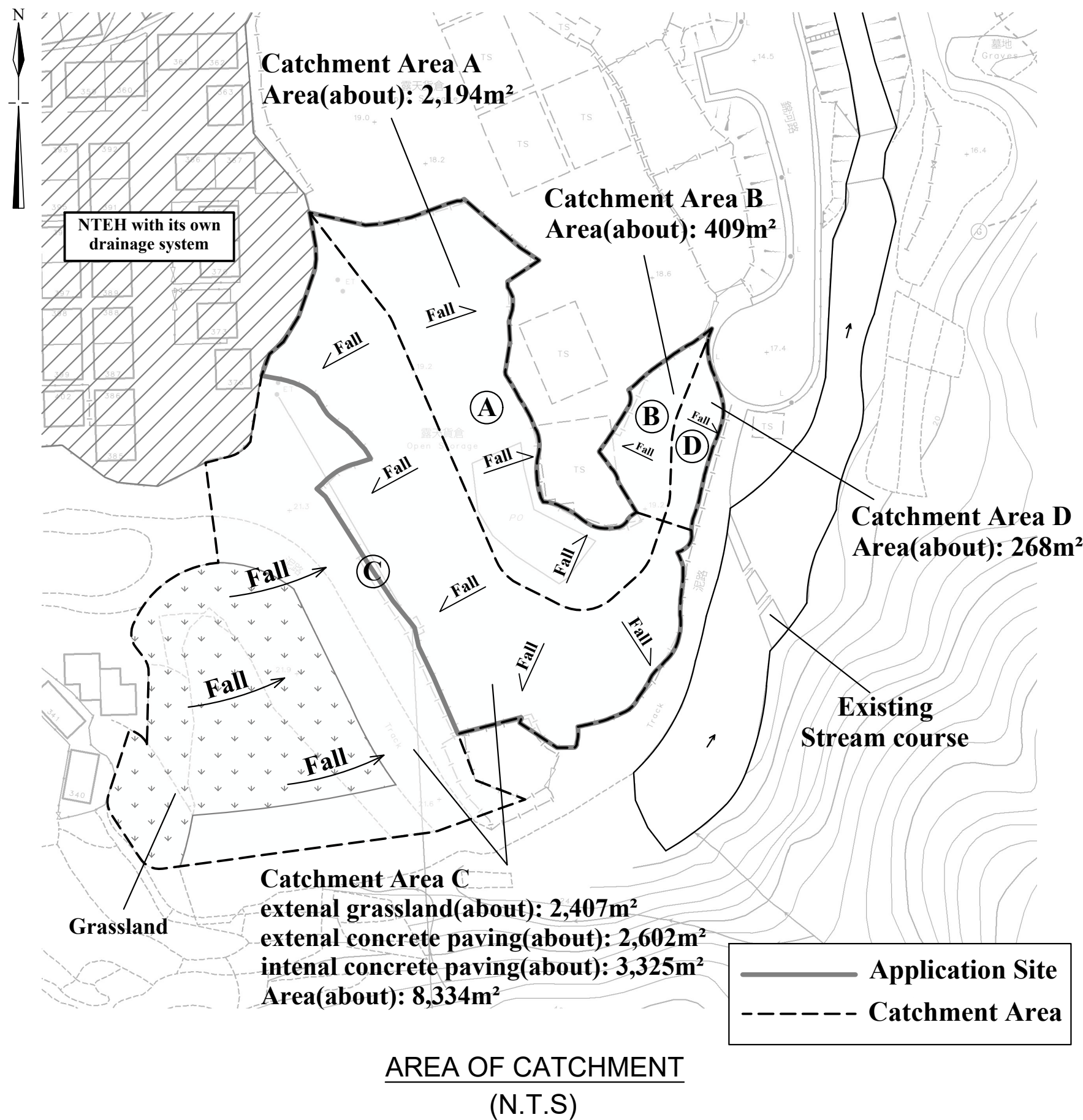
Francis Lau

Encl.

c.c.

DPO/FS&YLE, PlanD (Attn.: Mr. Thomas LAU)





N.T.S

January 2026

Drainage Proposal

Lots 1012 S.B, 1012 S.C, 1013, 1014RP, 1015 S.A, 1015 S.B,
1015 RP, 1016(part), 1018, 1034(part) and 1035 in D.D. 113
Yuen Long, N.T.

Goldrich Planners &
Surveyors Ltd.

Plan 6.2b
(P 25012)

Viewpoint Photo 1



(Photo taken on 7.1.2026)

Viewpoint Photo 2



River

(Photo taken on 7.1.2026)

Ref.

SDM 7.5.2 (d)

SDM 7.5.2 (d)

SDM 8.2.1

SDM 7.5.2 (d)

SDM Table 13
SDM Table 12

SDM 7.5.2 (d)

SDM 4.3.2
Corrigendum 1/2024
SDM Table 3a

SDM 7.5.2 (b)

SDM 7.5.2 (a)
Corrigendum 1/2022

SDM 7.5.2 (a)
Corrigendum 1/2022

SDM 7.5.2 (a)
Corrigendum 1/2022

Hydraulic Calculation

Goldrich Planners &
Surveyors Ltd.

Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP,
1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long,
New Territories

Page 1
(P25012)

1 For Catchment Area B			Ref.	
Area, A	=	409 m ²		
Average slope, H	=	0.1 m per 100m		
Distance on the line of natural flow, L	=	12 m		
Time of concentration, t ₀	=	$0.14465L / (H^{0.2}A^{0.1}) = 0.14465 (12) / (0.1^{0.2} \times 409^{0.1})$	SDM 7.5.2 (d)	
	=	1.5 min		
2 For Proposed UC in Catchment Area B				
	From	To		
Ground level (mPD)	18.70	19.20		
Invert level (mPD)	17.88	17.67		
Width of u-channel, w	=	750 mm		
Length of u-channel, L _c	=	42.5 m		
Depth of vertical part of u-channel, d	=	1155 mm		
Gradient of u-channel, S _f	=	$(17.88-17.67)/42.5 = 0.005$		
Cross-Section Area, a	=	$0.5 \pi r^2 + w d = 0.5 \times 3.14 \times 375^2 + 750 \times 1155$		
	=	1.087 m ²	SDM 8.2.1	
Wetted Perimeter, p	=	$\pi r + 2 d = 3.14 \times 375 + 2 \times 1155$		
	=	3.488 m		
Hydraulic radius, R	=	a / p		
	=	0.312 m		
3 Use Manning Equation for estimating velocity of stormwater				
Take n	=	0.016 for concrete lined channels:-	SDM Table 13	
Allowable velocity, v	=	$R^{1/6} \times (RS_f)^{1/2} / n = (0.312)^{1/6} \times (0.312 \times 0.005)^{1/2} / 0.016$	SDM Table 12	
	=	2.02 m/s		
Time of flow, t _f	=	0.4 min		
4 Use "Rational Method" for calculation of design flow				
Design intensity, i	=	$a / (t_0 + t_f + b)^c$	SDM 4.3.2	
	=	$505.5 / (1.5+0.4+3.29)^{0.355}$ for return period T = 50 years	Corrigendum 1/2024	
	=	283	SDM Table 3a	
Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A	SDM 7.5.2 (b)
Flat Grassland(heavy soil)	0.25	0.0	0.0	
Concrete Paving	0.95	409.0	388.6	
		SUM =	388.6	
Upstream flow, Q _u	=	0 m ³ /s		
Design flow, Q _d	=	$0.278i \sum C_i A_i + Q_u$ where A _i is in km ²	SDM 7.5.2 (a)	
	=	$1.16 \times 0.278 \times 283 \times 388.55 / 1000000 + 0$	Corrigendum 1/2022	
	=	0.035 m ³ /s		
Allowable flow, Q _a	=	a x v		
	=	1.087 x 2.02		
	=	2.196 m ³ /s		
	>	Q _d (O.K.)		
Reference was made to Stormwater Drainage Manual (SDM) by DSD				
Scale: NA	Hydraulic Calculation		Goldrich Planners & Surveyors Ltd.	
January 2026	Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP, 1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long, New Territories		Page 2 (P25012)	

1 For Connection between CP5 and CP14 <div> <div>Area, A = 0 m²</div> <div>Average slope, H = 0.1 m per 100m</div> <div>Distance on the line of natural flow, L = 0 m</div> </div> <div> <div>Time of concentration, t₀ = 0.14465 L / (H^{0.2} A^{0.1}) = 0.14465 (0) / (0.1^{0.2} 0^{0.1})</div> <div>= 0.0 min</div> </div>			Ref.																								
2 For Proposed Pipe after CP5 <div> <div>Size(Diameter) w = 600 mm</div> <div>Length of Pipe = 6 m</div> </div> <div>Design the pipe to 9/10 full bore capacity, then</div> <div>Area of ventilated portion = 0.1 of pipe area</div> <div> $\frac{1}{2} r^2 \theta - \frac{1}{2} r^2 \sin(\theta)$ = 0.1 πr^2 $\theta - \sin(\theta)$ = 0.2 π θ = 1.63 rad = 93.4° (By trial and error) </div> <div> <div>Area A = 0.9 πr^2</div> <div>= 0.9 x 3.14 x 600²</div> <div>= 1017360 mm²</div> <div>= 1.017 m²</div> </div> <div> <div>Wetted Perimeter P = 2 $\pi r - r \theta$ = 2792 mm</div> <div>Hydraulic radius R = $\frac{A}{P}$</div> <div>= 364.4 mm</div> </div>			SDM 7.5.2 (d)																								
3 Use Manning Equation for estimating velocity of stormwater <div> <div>Fall S = 1: 200</div> <div>Take n = 0.016 for concrete lined channels:-</div> </div> <div> <div>Allowable velocity, v = $R^{1/6} \times (RS)^{1/2} / n$ = (0.364)^{1/6} * (0.364/200)^{1/2} / 0.016</div> <div>= 2.25 m/s</div> </div> <div>Time of flow, t_f = 0.04 min</div>			SDM 8.2.1																								
4 Use "Rational Method" for calculation of design flow <div> <div>Design intensity, i = a / (t₀ + t_f + b)^c</div> <div>= 505.5 / (0.0+0.04+3.29)^{0.355} for return period T = 50 years</div> <div>= 330</div> </div> <table> <tr> <th>Type of surface</th><th>Runoff Coefficient C</th><th>Catchment Area A (m²)</th><th>C x A</th></tr> <tr> <td>Flat Grassland (heavy soil)</td><td>0.25</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Concrete Paving</td><td>0.95</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Macadam Roadways</td><td>0.425</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Wooded Areas</td><td>0.105</td><td>0.0</td><td>0.0</td></tr> <tr> <td colspan="3">SUM =</td><td>0.0</td></tr> </table> <div> <div>Upstream flow, Q_u = 0.209 m³/s</div> <div>Design flow, Q_d = 0.278i $\Sigma C_i A_i$ + Q_u where A_i is in km²</div> <div>= 1.16 x 0.278 x 330 x 0 / 1000000 + 0.209</div> <div>= 0.209 m³/s</div> <div>Allowable flow, Q_a = a x v</div> <div>= 1.02 x 2.25</div> <div>= 2.294 m³/s</div> <div>> Q_d (O.K.)</div> </div>			Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A	Flat Grassland (heavy soil)	0.25	0.0	0.0	Concrete Paving	0.95	0.0	0.0	Macadam Roadways	0.425	0.0	0.0	Wooded Areas	0.105	0.0	0.0	SUM =			0.0	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a
Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A																								
Flat Grassland (heavy soil)	0.25	0.0	0.0																								
Concrete Paving	0.95	0.0	0.0																								
Macadam Roadways	0.425	0.0	0.0																								
Wooded Areas	0.105	0.0	0.0																								
SUM =			0.0																								
Reference was made to Stormwater Drainage Manual (SDM) by DSD			SDM 7.5.2 (b)																								
Scale: NA	Hydraulic Calculation Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP, 1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long, New Territories	Goldrich Planners & Surveyors Ltd.																									
January 2026		Page 3 (P25012)																									

1 For Catchment Area C			Ref.
Area, A	=	8334 m ²	SDM 7.5.2 (d)
Average slope, H	=	0.1 m per 100m	
Distance on the line of natural flow, L	=	35 m	
Time of concentration, t _o	=	$0.14465L / (H^{0.2}A^{0.1}) = 0.14465 (35) / (0.1^{0.2} \times 8334^{0.1})$ = 3.3 min	
2 For Proposed UC in Catchment Area C			SDM 8.2.1
	From	To	
Ground level (mPD)	19.40	19.20	
Invert level (mPD)	18.65	17.64	
Width of u-channel, w	=	750 mm	SDM 8.2.1
Length of u-channel, L _c	=	203 m	
Depth of vertical part of u-channel, d	=	1185 mm	
Gradient of u-channel, S _f	=	$(18.65-17.64)/203 = 0.005$	
Cross-Section Area, a	=	$0.5 \pi r^2 + w d = 0.5 \times 3.14 \times 375^2 + 750 \times 1185$ = 1.110 m ²	SDM 8.2.1
Wetted Perimeter, p	=	$\pi r + 2 d = 3.14 \times 375 + 2 \times 1185$ = 3.548 m	
Hydraulic radius, R	=	a / p = 0.313 m	
3 Use Manning Equation for estimating velocity of stormwater			SDM Table 13 SDM Table 12
Take n	=	0.016 for concrete lined channels:-	
Allowable velocity, v	=	$R^{1/6} \times (RS_f)^{1/2} / n = (0.313)^{1/6} \times (0.313 \times 0.005)^{1/2} / 0.016$ = 2.03 m/s	
Time of flow, t _f	=	1.7 min	
4 Use "Rational Method" for calculation of design flow			SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a
Design intensity, i	=	$a / (t_o + t_f + b)^c$ = $505.5 / (3.3+1.7+3.29)^{0.355}$ for return period T = 50 years = 239	
Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	
Flat Grassland (heavy soil)	0.25	2407.0	
Concrete Paving	0.95	5927.0	SDM 7.5.2 (b)
		SUM = 6232.4	
Upstream flow, Q _u	=	0 m ³ /s	
Design flow, Q _d	=	$0.278i \sum C_i A_i + Q_u$ where A _i is in km ² = $1.16 \times 0.278 \times 239 \times 6232.4 / 1000000 + 0$ = 0.481 m ³ /s	SDM 7.5.2 (a) Corrigendum 1/2022
Allowable flow, Q _a	=	$a \times v$ = 1.11×2.03 = 2.254 m ³ /s	
	>	Q _d (O.K.)	
Reference was made to Stormwater Drainage Manual (SDM) by DSD			
Scale: NA	Hydraulic Calculation		Goldrich Planners & Surveyors Ltd.
January 2026	Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP, 1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long, New Territories		Page 4 (P25012)

Ref.

$$\text{Time of concentration, } t_o = 0.14465 \text{ L} / (\text{H}^{0.2} \text{A}^{0.1}) = 0.14465 (10) / (0.1^{0.2} \times 268^{0.1})$$

$$= 1.3 \text{ min}$$

SDM 7.5.2 (d)

SDM 8.2.1

Width of u-channel, w = 750 mm
 Length of u-channel, L_c = 37.5 m
 Depth of vertical part of u-channel, d = 1185 mm
 Gradient of u-channel, S_f = $(17.83-17.64)/37.5 = 0.005$

$$\text{Wetted Perimeter, } p = \pi r + 2d = 3.14 \times 375 + 2 \times 1185 = 3.548 \text{ m}$$

Hydraulic radius, $R = a / p$
 $= 0.313 \text{ m}$

SDM Table 12

Take $n = 0.016$ for concrete lined channels:-
 Allowable velocity, $v = R^{1/6} \times (RS_f)^{1/2} / n = (0.313)^{1/6} \times (0.313 \times 0.005)^{1/2} / 0.016$
 $= 2.05 \text{ m/s}$
 Time of flow, $t_f = 0.3 \text{ min}$

SDM 4.3.2
Corrigendum 1/2024
SDM Table 3a

Design intensity, $i = a / (t_o + t_f + b)^c$
 $= 505.5 / (1.3 + 0.3 + 3.29)^{0.355}$ for return period $T = 50$ years
 $= 287$

Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A
Flat Grassland (heavy soil)	0.25	0.0	0.0
Concrete Paving	0.95	268.0	254.6
		SUM =	254.6

Upstream flow, $Q_{11} = 0 \text{ m}^3/\text{s}$

$$\begin{aligned}\text{Design flow, } Q_d &= 0.278i \sum C_f A_i + Q_u \quad \text{where } A_i \text{ is in km}^2 \\ &= 1.16 \times 0.278 \times 287 \times 254.6 / 1000000 + 0 \\ &= 0.024 \text{ m}^3/\text{s}\end{aligned}$$

$$\begin{aligned}\text{Allowable flow, } Q_a &= a \times v \\ &= 1.11 \times 2.05 \\ &= 2.274 \text{ m}^3/\text{s}\end{aligned}$$

> Q_d (O.K.)

Reference was made to Stormwater Drainage Manual (SDM) by DSD

Scale: NA

Hydraulic Calculation

Goldrich Planners &
Surveyors Ltd.

January 2026

Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP,
1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long,
New Territories

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1 For Connection between CP14 to existing river <div style="display: flex; justify-content: space-between;"> <div> Area, A = 0 m² Average slope, H = 0.1 m per 100m Distance on the line of natural flow, L = 0 m </div> <div> Time of concentration, $t_o = 0.14465L / (H^{0.2}A^{0.1}) = 0.14465 (0) / (0.1^{0.2} \times 0^{0.1})$ = 0.0 min </div> </div>			Ref.																								
2 For Pipe after Cp14 <div style="display: flex; justify-content: space-between;"> <div> Size(Diameter) w = 600 mm Length of Pipe = 12 m Design the pipe to 9/10 full bore capacity, then Area of ventilated portion = 0.1 of pipe area $\frac{1}{2} r^2 \theta - \frac{1}{2} r^2 \sin(\theta) = 0.1 \pi r^2$ $\theta - \sin(\theta) = 0.2 \pi$ $\theta = 1.63$ rad = 93.4° (By trial and error) </div> <div> Area A = $0.9 \pi r^2$ = $0.9 \times 3.14 \times 600^2$ = 1017360 mm² = 1.017 m² </div> </div> <div style="display: flex; justify-content: space-between; margin-top: 10px;"> <div> Wetted Perimeter P = $2 \pi r - r \theta$ Hydraulic radius R = A/P = 364.4 mm </div> <div>= 2792 mm</div> </div>			SDM 7.5.2 (d)																								
3 Use Manning Equation for estimating velocity of stormwater <div style="display: flex; justify-content: space-between;"> <div> Fall S = 1: 200 Take n = 0.016 for concrete lined channels:- Allowable velocity, v = $R^{1/6} \times (RS)^{1/2} / n = (0.364)^{1/6} \times (0.364/200)^{1/2} / 0.016$ = 2.25 m/s Time of flow, $t_f = 0.089$ min </div> </div>			SDM 8.2.1																								
4 Use "Rational Method" for calculation of design flow <div style="display: flex; justify-content: space-between;"> <div> Design intensity, i = $a / (t_o + t_f + b)^c$ = $505.5 / (0.0 + 0.09 + 3.29)^{0.355}$ = 328 </div> <div>for return period T = 50 years</div> </div> <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 10px;"> <thead> <tr> <th>Type of surface</th><th>Runoff Coefficient C</th><th>Catchment Area A (m²)</th><th>C x A</th></tr> </thead> <tbody> <tr> <td>Flat Grassland (heavy soil)</td><td>0.25</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Concrete Paving</td><td>0.95</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Macadam Roadways</td><td>0.425</td><td>0.0</td><td>0.0</td></tr> <tr> <td>Wooded Areas</td><td>0.105</td><td>0.0</td><td>0.0</td></tr> <tr> <td colspan="3" style="text-align: right;">SUM =</td><td>0.0</td></tr> </tbody> </table> <div style="margin-top: 10px;"> Upstream flow, $Q_u = 0.714$ m³/s Design flow, $Q_d = 0.278i \sum C_i A_i + Q_u$ where A_i is in km² = $1.16 \times 0.278 \times 328 \times 0 / 1000000 + 0.714$ = 0.714 m³/s Allowable flow, $Q_a = a \times v$ = 1.02×2.25 = 2.294 m³/s > Q_d (O.K.) </div>			Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A	Flat Grassland (heavy soil)	0.25	0.0	0.0	Concrete Paving	0.95	0.0	0.0	Macadam Roadways	0.425	0.0	0.0	Wooded Areas	0.105	0.0	0.0	SUM =			0.0	SDM 4.3.2 Corrigendum 1/2024 SDM Table 3a
Type of surface	Runoff Coefficient C	Catchment Area A (m ²)	C x A																								
Flat Grassland (heavy soil)	0.25	0.0	0.0																								
Concrete Paving	0.95	0.0	0.0																								
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SUM =			0.0																								
Reference was made to Stormwater Drainage Manual (SDM) by DSD			SDM 7.5.2 (b)																								
Reference was made to Stormwater Drainage Manual (SDM) by DSD			SDM 7.5.2 (a) Corrigendum 1/2022																								
Scale: NA	Hydraulic Calculation <small>Lots 1012 S.B, 1012 S.C, 1013, 1014 RP, 1015 S.A, 1015 S.B, 1015 RP, 1016 (Part), 1018, 1034 (Part) and 1035 in D.D.113, Kam Tin, Yuen Long, New Territories</small>	Goldrich Planners & Surveyors Ltd.																									
January 2026		Page 6 (P25012)																									